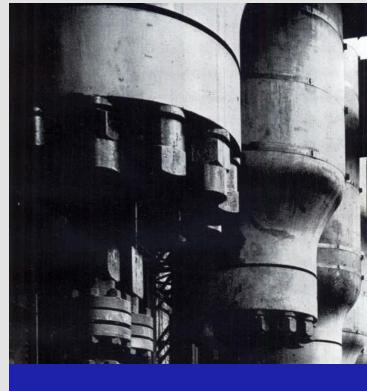


# Technology and catalyst development



**Historic HP Converters** 

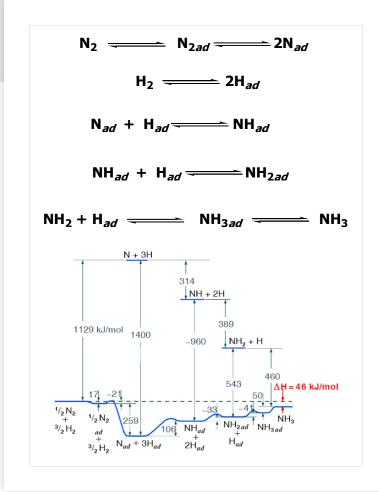


Fused Fe-ammonia synthesis catalyst



## Ammonia synthesis

Consider  $3H_2 + N_2 \rightarrow 2NH_3$  at  $400-500^{\circ}C$  (750-932°F), 200 bar (2900 psi)



Reactor size

Daily NH<sub>3</sub>

make



**A?** 

**Catalyst** 

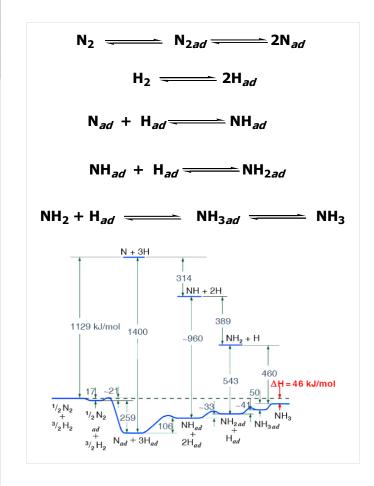


**B?** 



# Ammonia synthesis

Consider  $3H_2 + N_2 \rightarrow 2NH_3$  at  $400-500^{\circ}C$  (750-932°F), 200 bar (2900 psi)



Reactor size



Daily NH<sub>3</sub> make

0.1 g

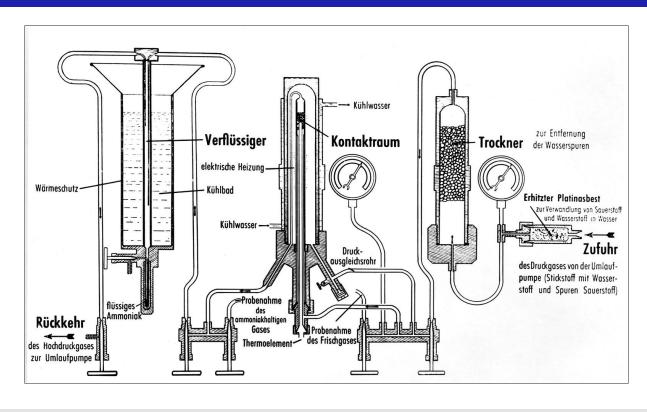
Catalyst

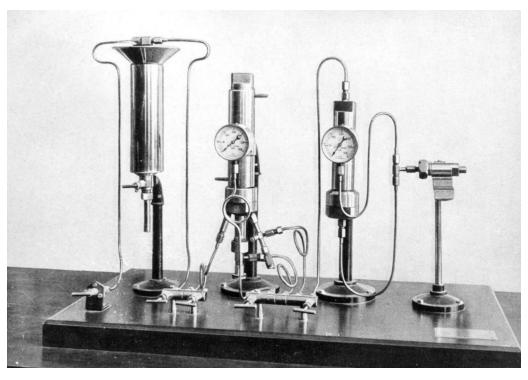


3,500 tpd

# First continuous ammonia process (1909)

Process was and remains a loop

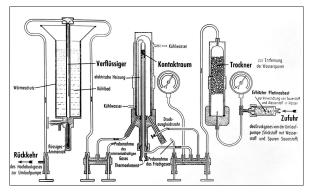




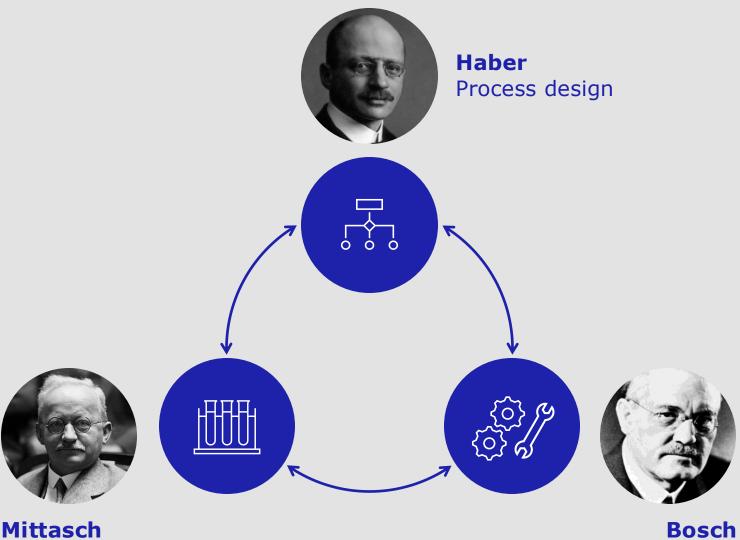


# Teamwork – a mix of skills





1908 Laboratory scale 1913 Production scale



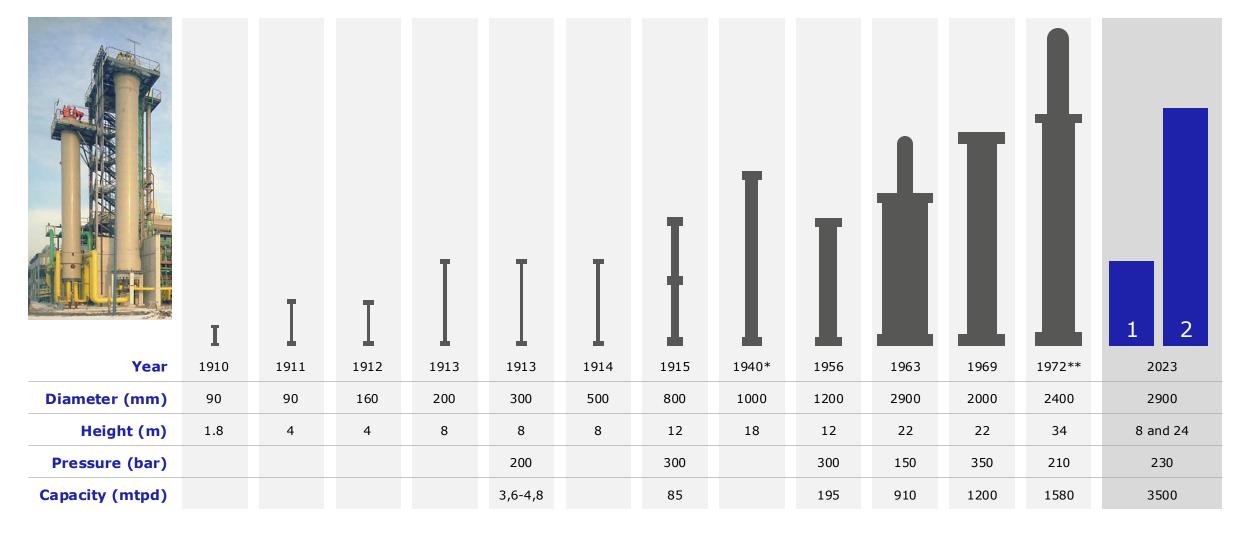
**Mittasch** Catalyst chemistry

Mechanical design



# Reactor development – ammonia synthesis

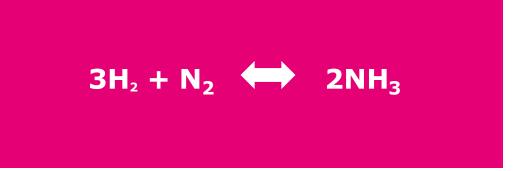
#### Economies of scale





# Ammonia chemistry

### **Reaction: (exothermic)**



 $\Delta H_{298} = -46 \text{ kJ/mol NH}_3$ 

### **Favoured by:**



Capex, opex

#### Low temperature

Kinetics vs equilibrium

Low inlet ammonia concentration

Low inert levels - Ar, CH<sub>4</sub>, He, etc.



# Effect of temperature

### **At low temperature:**

### At high temperature:

Rate of reaction is slow (kinetic limit)

Rate of reaction is slow (equilibrium limit)

### Hence:

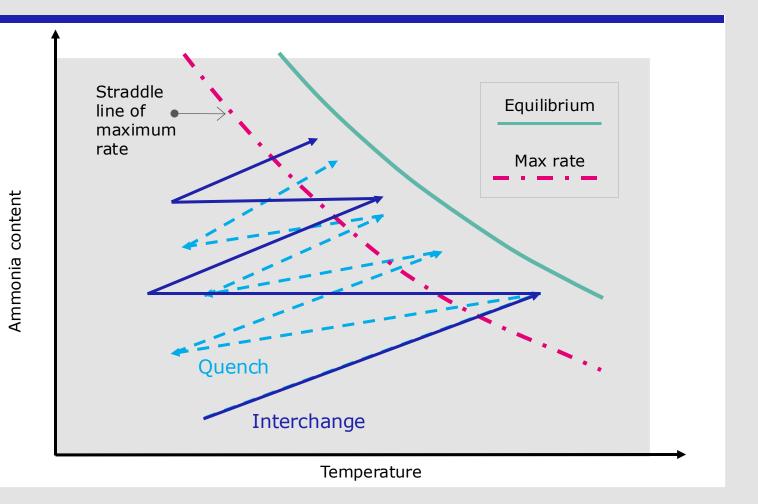
Rate of reaction passes through a maximum as temperature increases







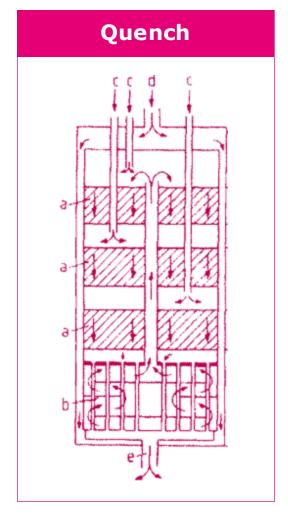
# Converters – ammonia synthesis reactors

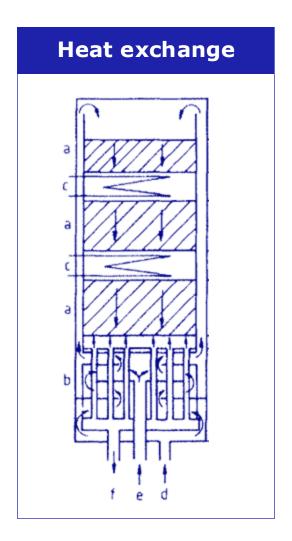


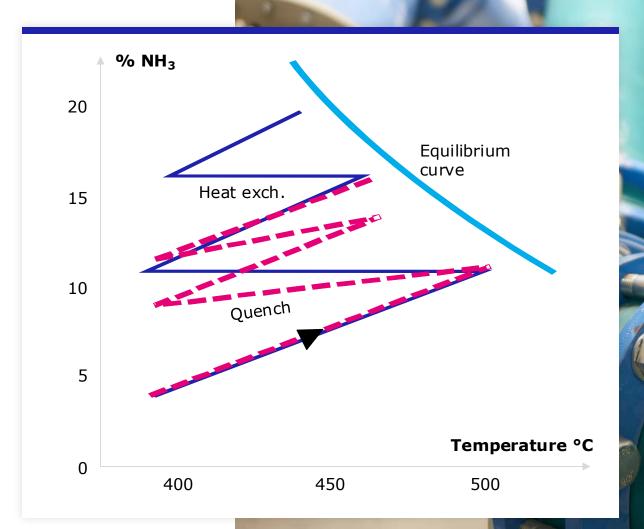




# Reactor development – ammonia synthesis

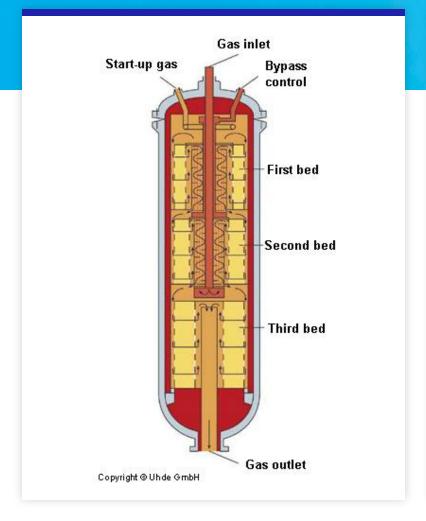








# Reactor development - ammonia synthesis



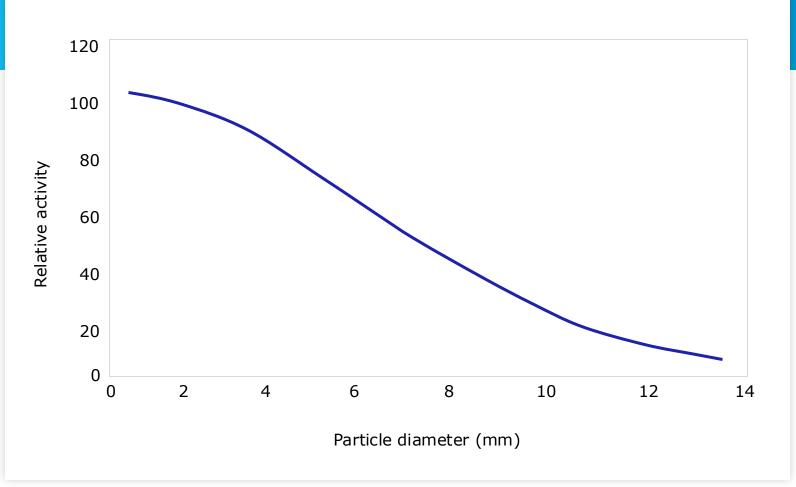
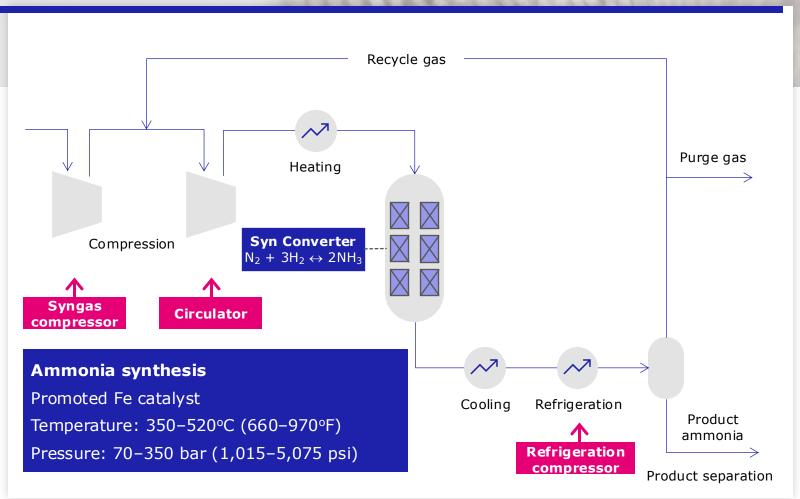
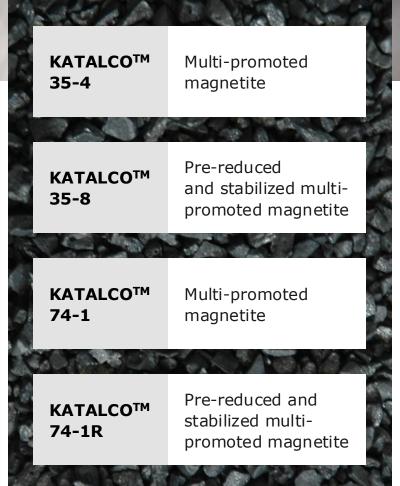




Image: tk Uhde

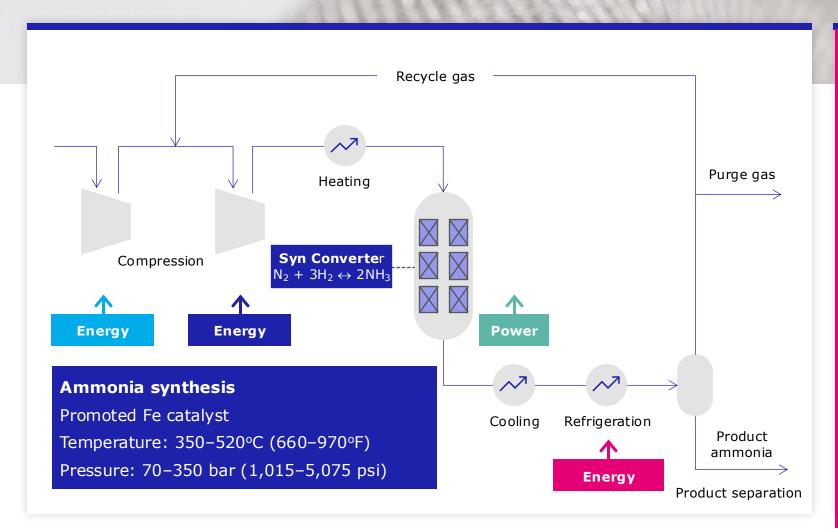
# Synthesis loop







## Synthesis loop – energy demand



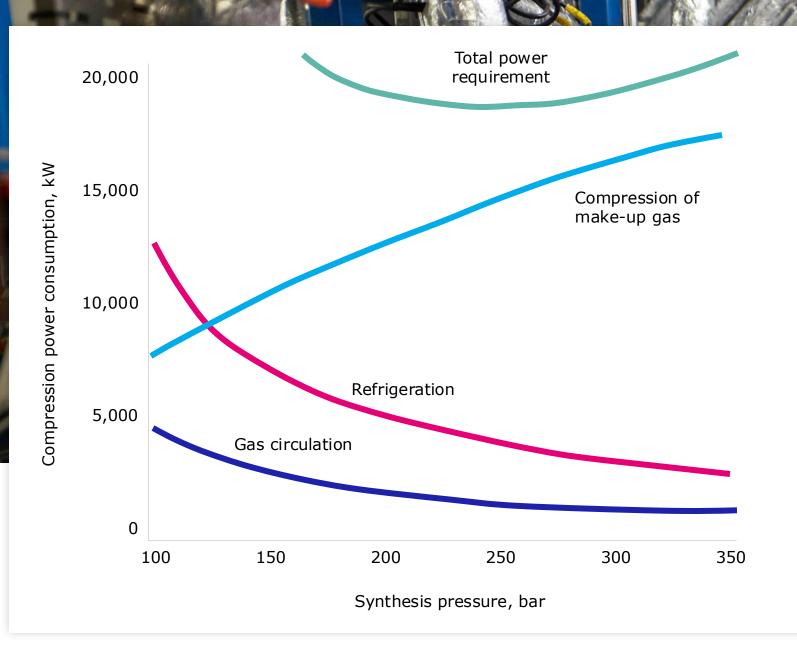
#### Interactions between:-

- loop operating pressure
- refrigeration level
- circulation rate

Give **total power required** to drive machinery.

Lower pressures require more power for refrigeration and recirculation.







Typically loop designs 130 - 220 bar (1,900 - 3,200psi)

### Optimum conditions – swings and roundabouts...

#### **Pressure**

Increased pressure gives:

- Increased ammonia content
- Increased compressor power
- Reduced circulator power
- Reduced refrigeration power
- Non-linear effect on capex

Flat optimum, most plants between 130 bar and 220 bar (1,900 – 3,190 psi)

#### **Temperature**

Catchpot removes ammonia from the loop

Lower catchpot temperature

- More ammonia removed per pass
- Less ammonia recycled to converter
- More ammonia made in the converter

#### But

Increased refrigeration duty

No impact on overall conversion



### Moisture

### Moisture poisons ammonia synthesis catalyst

#### **Moisture comes from**

 $H_2O$ 

$O_2 + 2H_2 \rightarrow 2H_2O$	Rarely present

 $CO + 3H_2 \rightarrow CH_4 + H_2O$  Remove by methanation

 $CO_2 + 4H_2O \rightarrow CH_4 + 2H_2O$  Remove by methanation

#### Water removed as follows...

#### **Before the loop**

- Syn Gas Driers
- Ammonia Wash

#### In the loop

Add make-up gas before the catchpot / refrigeration system and let water leave with the ammonia product stream





# Synthesis loop purge



#### Ar

Air added to secondary

#### **CH**₄

CH<sub>4</sub> slip from secondary reformer Methanated CO slip from LTS Methanated CO<sub>2</sub> slip from CO<sub>2</sub> removal unit

#### **Sometimes He**

Natural gas



Lower partial pressure of H<sub>2</sub> and N<sub>2</sub> Lower ammonia conversion

### Removed by purging

### Purge contains ~65% H<sub>2</sub>

High inerts in MUG

- → High purge
- → Loss of hydrogen
- → Less ammonia



### H<sub>2</sub> recovery

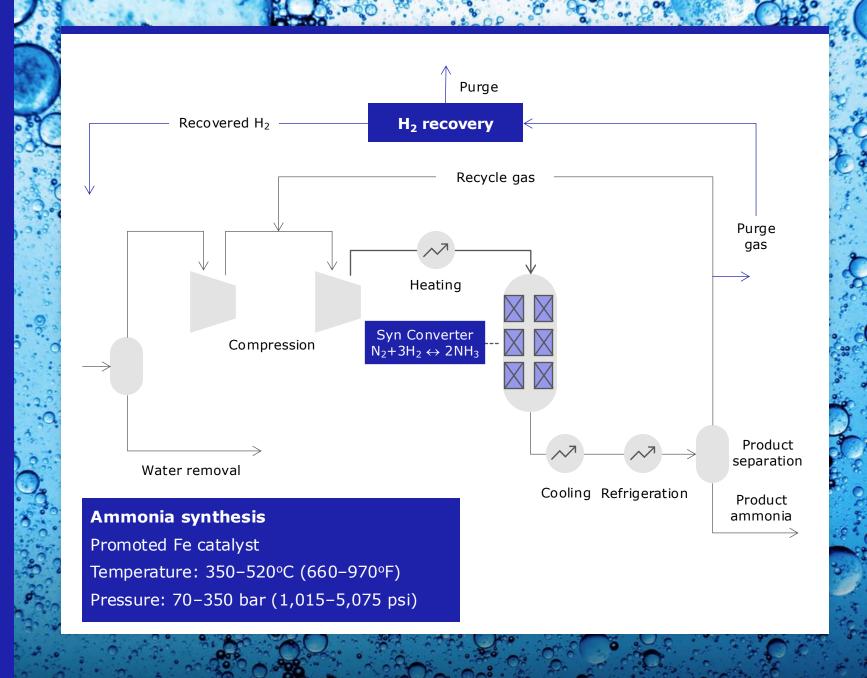
# Most plants recover H<sub>2</sub> from the loop purge

- Cryogenic
- Membrane
- PSA (less common)

Overall performance is similar, typically 90% H<sub>2</sub> recovery at 90% purity

Overall loop H<sub>2</sub> conversion to NH<sub>3</sub> increases from about 92% to 98%

MUG H / N ratio changes from 3.0 to approx. 2.85, and returns to 3.0 after  $H_2$  addition





### Activity decreases with time



Loop pressure increases

- Efficiency reduced
- No effect on throughput

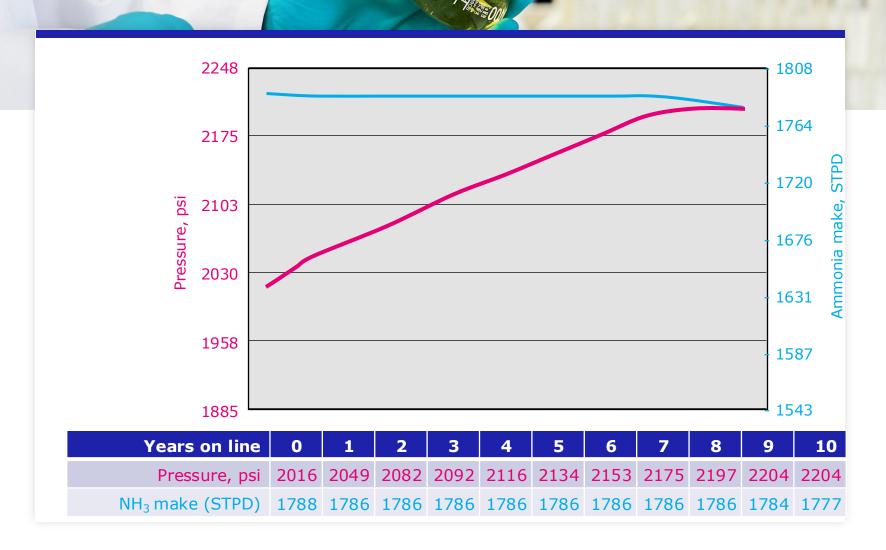
Throughput affected when loop limit encountered

• E.g., relief valve setting

Converter can become more difficult to restart and more sensitive to plant upsets

Efficiency loss, typically

- 0.1-0.2GJ/te
- 0.095-0.19mmBTU/te





### **Formulation**

### Magnetite (Fe<sub>3</sub>O<sub>4</sub>) precursor

#### **Controlled reduction**

Pre-reduction or in situ reduction

Oxygen is removed from the crystal lattice without shrinkage

Produces extremely porous metallic iron structure

Key to achieving a high activity catalyst

**Promoters boost catalyst performance** 



# Effect of promoters and stabilisers



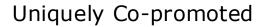
Promoter	Effect
$Al_2O_3$	Stabilises the internal surface
MgO	Increases the thermal stability
SiO <sub>2</sub>	Stabilises activity in presence of oxygen compounds during normal operation and reduction
K <sub>2</sub> O	Increases intrinsic activity of Fe particles
CaO	Protects the K promoter against neutralisation and increases the stability against poisoning by sulphur
CoO	Increases intrinsic activity <b>KATALCO</b> 74-1





# Ammonia synthesis

### **KATALCO 74-1**



Most active Fe-catalyst

Largest plants use it

Lowest pressure commercial reference

Has replaced high activity Ruthenium catalyst

Achieved lives of >20 years

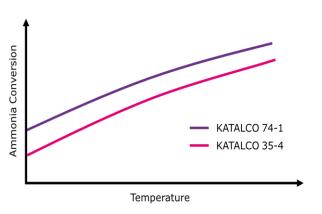


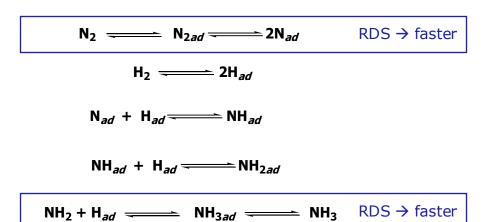


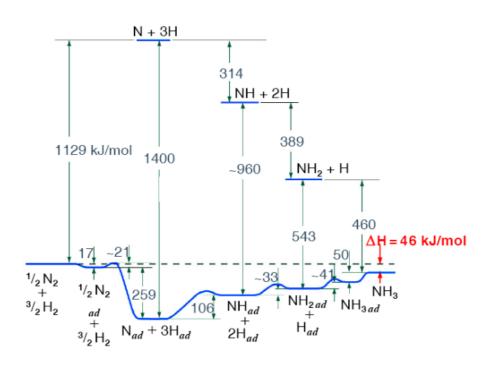
## Ammonia synthesis

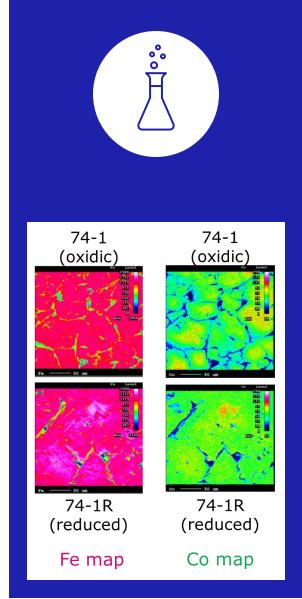
#### **KATALCO 74-1**

Unique cobalt promotion
Increases activity
Increases reaction rates
High stability











### **KATALCO** 74-1 Koch Fort Dodge low pressure reference

#### Recent North American reference

14 Jun 2023 09:00

thyssenkrupp Uhde and Johnson Matthey increase ammonia synthesis capacity at Koch Fertilizer facility



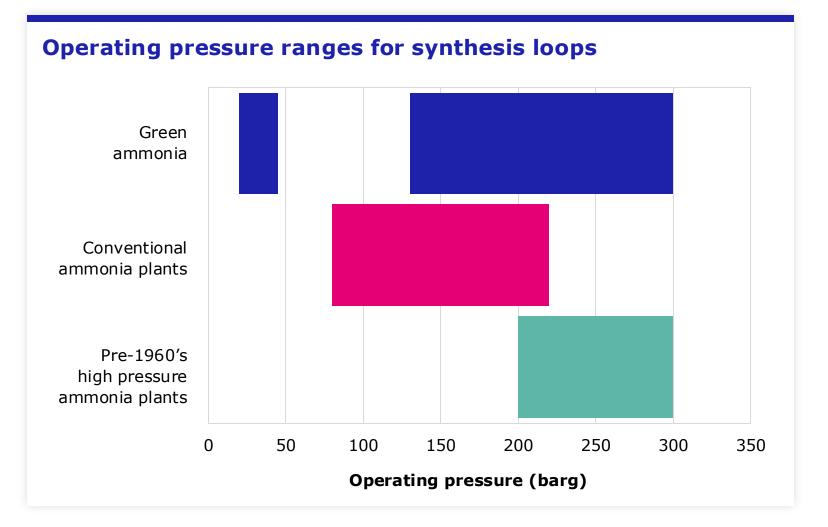
Koch Fertilizer facility, Fort Dodge, Iowa (USA

For this revamp to increase capacity a key challenge was the **very low** ammonia synthesis **operating pressure** of **only 960 psig / 66 barg** for the ammonia synthesis converter

Solved by combining high-performance catalyst **KATALCO** 74-1 with an adapted novel process design from thyssenkrupp Uhde

This joint solution has enabled the increased ammonia synthesis capacity

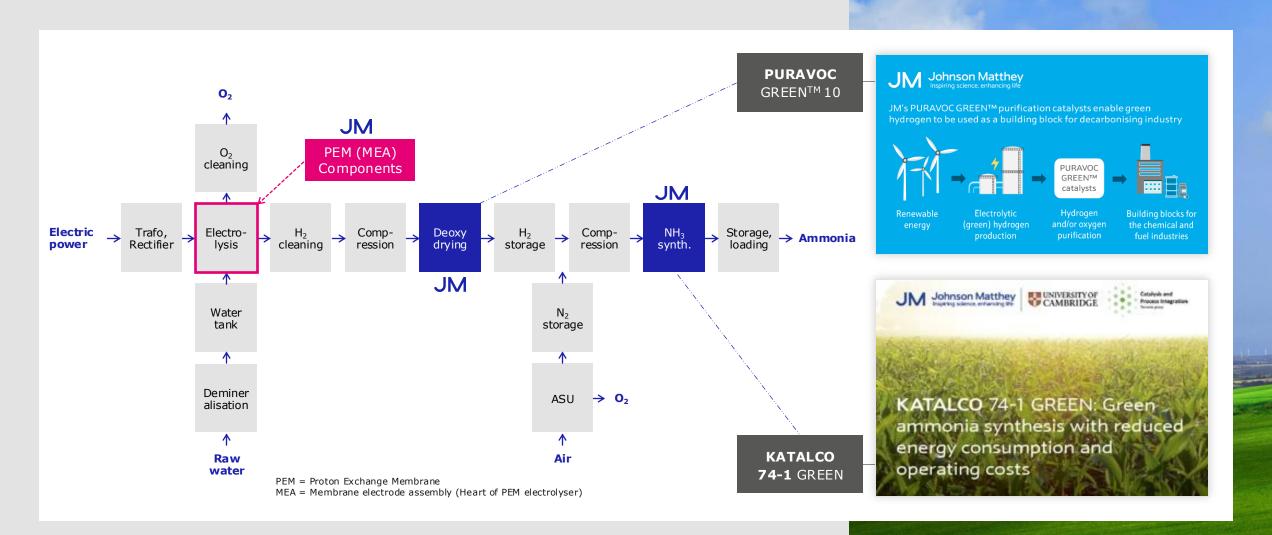
# Green ammonia technologies in development



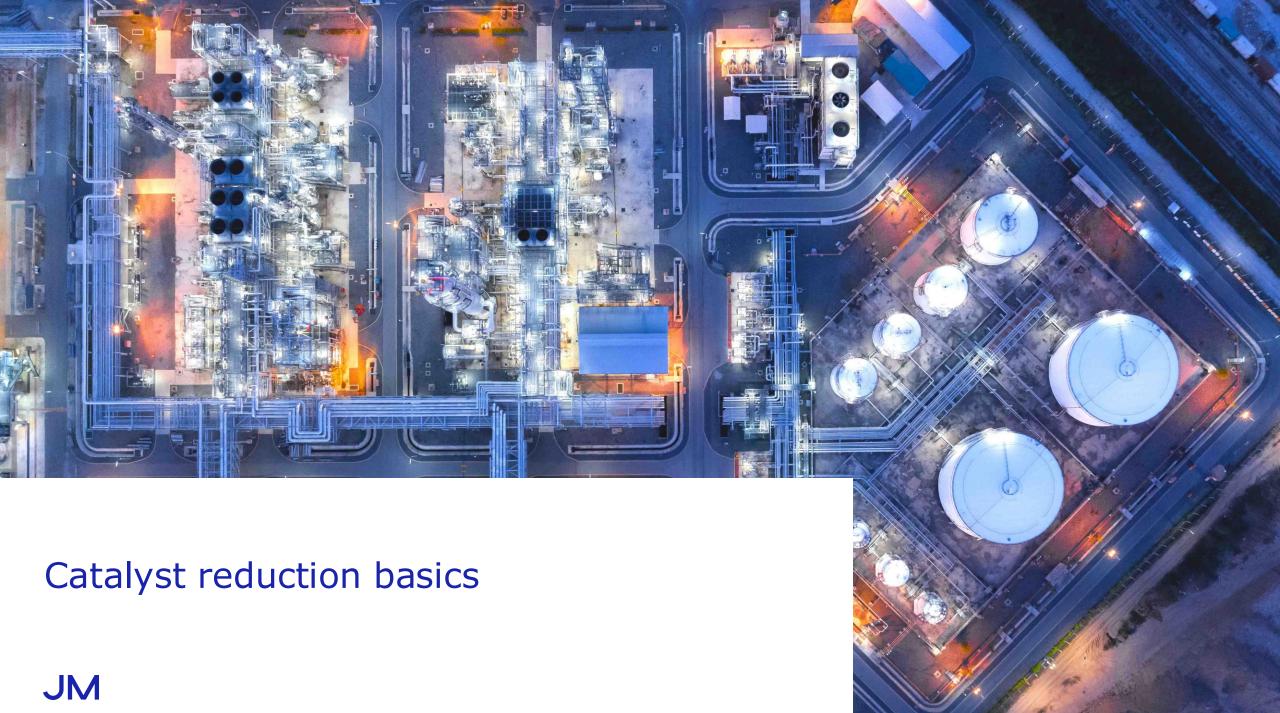




## JM GREEN ammonia products







## Catalyst reduction and pre-reduction

#### **Conversion of magnetite to active iron**

Promoters migrate and protect against sintering

Oxygen removed with no change in crystal size

Surface area increases from 0.02 to ~18m<sup>2</sup>g<sup>-1</sup> providing active sites

#### **Reduction water and recycled water are poisons**

#### Reduction with H<sub>2</sub>

No ammonia

All heat from start-up heater → Slow

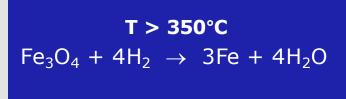
Circulator design

#### **Reduction with syngas**

Ammonia formed → reduction liquor

Heat of reaction  $\rightarrow$  fast

Making product whilst still reducing







## Pre-reduced catalyst

### How long does catalyst reduction take?

A good crew can reduce a charge of synthesis catalyst in 4–5 days

Often times it takes 10 days

Some examples >20 days

### **Pre-reduced catalyst**

- 1-2 days for reduction
- 2x the cost

### **Usual compromise is**

- One bed of pre-reduced
- All other beds are oxidic



# Ammonia synthesis summary



<b>Topics of interest</b>	Comment
Key variables	<ul> <li>Inlet temperature</li> <li>Exit temperature</li> <li>PD</li> </ul>
Good performance indicators	<ul> <li>Profile</li> <li>Loop pressure</li> <li>Exit ammonia conc</li> </ul>
Common issues	<ul> <li>Mechanical issue with cartridge</li> <li>CO/CO<sub>2</sub>/H<sub>2</sub>O poisoning</li> </ul>
End of life criteria	<ul> <li>Loop pressure</li> <li>Mechanical issue with cartridge</li> <li>Replace with better cartridge</li> </ul>
Optimisation	Inlet bed temperatures



